



## 5 Project Planning for Gear Units

### 5.1 Efficiency of gear units

The efficiency of the gear unit is mainly determined by the gearing and bearing friction. Note that the starting efficiency of a gear unit is always less than its efficiency at operating speed.

The efficiency of MC.. helical and bevel-helical gear units varies depending on the number of gear stages.

Based on nominal power, the efficiency  $\eta$  is roughly:

- MC2P: 0.97
- MC3P: 0.955
- MC2R: 0.97
- MC3R: 0.955

### 5.2 Service factor $F_S$ , peak factor $F_F$

**Service factor  $F_S$**  The service factor takes into account the load impacts generated by the driving motor and the driven machine.

Recommended values in respect to

- field of application
- driven machine
- operating period / day

are given in the following table.

These tables are valid for **electric motors** used as driving machine.

For other types of driving machines, the following correction values apply:

- Combustion engines with four or more cylinders:  $F_S$  (selection table) + 0.25
- Combustion engines with one or three cylinders:  $F_S$  (selection table) + 0.5



Field of application/industry	Driven machine	Service factor operating period /day		
		< 3 h	3-10 h	> 10 h
<b>Agitators and mixers</b>	Agitators for liquids	1.00	1.25	1.50
	Agitators for liquids (variable density)	1.20	1.50	1.65
	Agitators for solids (non-uniform material)	1.40	1.60	1.70
	Agitators for solids (uniform material)	-	1.35	1.40
	Concrete mixers	-	1.50	1.50
<b>Cableways</b>	Material ropeways	-	1.40	1.50
	Aerial tramways	1) <sup>1)</sup>	1) <sup>1)</sup>	1) <sup>1)</sup>
	Surface lifts	1) <sup>1)</sup>	1) <sup>1)</sup>	1) <sup>1)</sup>
	Continuous aerial tramways	1) <sup>1)</sup>	1) <sup>1)</sup>	1) <sup>1)</sup>
	Funicular railway	1) <sup>1)</sup>	1) <sup>1)</sup>	1) <sup>1)</sup>
<b>Conveyors</b>	Bucket elevators	-	1.40	1.50
	Hoists - other	-	1.50	1.80
	Belt conveyors ≤ 100 kW	1.15	1.25	1.40
	Belt conveyors > 100 kW	1.15	1.30	1.50
	Apron feeders	-	1.25	1.50
	Screw feeders	1.15	1.25	1.50
	Shakers, reciprocating	1.55	1.75	2.00
	Escalators	1.55	1.25	1.50
	Passenger lifts	1) <sup>1)</sup>	1) <sup>1)</sup>	1) <sup>1)</sup>
<b>Compressors</b>	Reciprocating	-	1.80	1.90
	Centrifugal compressor	-	1.40	1.50
	screw-type	-	1.50	1.75
<b>Cranes and hoists</b>	Cranes and hoists	1) <sup>1)</sup>	2) <sup>2)</sup>	2) <sup>2)</sup>
<b>Energy</b>	Frequency converters	-	1.80	2.00
	Water wheels (low speed)	-	-	1.70
	Water turbines	-	-	1) <sup>1)</sup>
<b>Fans</b>	Heat exchangers	1.50	1.50	1.50
	Dry cooling towers	-	-	2.00
	Wet cooling towers	2.00	2.00	2.00
	Blowers (axial and radial)	1.50	1.50	1.50
<b>Food industry</b>	Crushers and mills	-	-	1.75
	Beet slicer	-	1.25	1.50
	Drying Drums	-	1.25	1.50
<b>Metal mills</b>	Winders	-	1.60	1.75
	Slitters	1.55	1.75	2.00
	Table conveyors, individual drives	1) <sup>1)</sup>	1) <sup>1)</sup>	1) <sup>1)</sup>
	Table conveyors, group drives	1) <sup>1)</sup>	1) <sup>1)</sup>	1) <sup>1)</sup>
	Table conveyors, reversing	1) <sup>1)</sup>	1) <sup>1)</sup>	1) <sup>1)</sup>
	Wire drawing machines	1.35	1.50	1.75
	Flattening machines	1) <sup>1)</sup>	1) <sup>1)</sup>	1) <sup>1)</sup>

1) Contact SEW-EURODRIVE

2) Contact SEW-EURODRIVE; dimensioning according to FEM1001



Field of application	Driven machine	Service factor operating period /day		
		< 3 h	3-10 h	> 10 h
<b>Mills and drums</b>	Dryers and coolers	-	1.50	1.60
	Kilns	-	-	2.00
	Ball mills	-	-	2.00
	Coal mills	-	1.50	1.75
<b>Pumps</b>	Centrifugal pumps	1.15	1.35	1.45
	Reciprocating (single-cylinder)	1.35	1.50	1.80
	Reciprocating (multi-cylinder)	1.20	1.40	1.50
	Spiral pumps	-	1.25	1.50
	Rotary (gear type, vane)	-	-	1.25
<b>Lumber industry</b>	Lumber industry	1)	1)	1)
<b>Mining industry</b>	Crushers	1.55	1.75	2.00
	Screens and shakers	1.55	1.75	2.00
	Slewing drives	-	1.55	1.80
	Dredgers	1)	1)	1)
<b>Pulp and paper industry</b>	Debarking Drums and Barkers	1.55	1.80	-
	Rolls (pick-up, wire drive, wire suction)	-	1.80	2.00
	Dryer cylinders (anti-friction bearings)	-	1.80	2.00
	Calenders (anti-friction bearings)	-	1.80	2.00
	Filters (pressure vacuum)	-	1.80	2.00
	Beaters and chippers	1.55	1.75	2.00
	Jordan mills	-	1.50	1.75
	Presses (bark, felt, size, suction)	-	-	1.75
	Reels	-	-	1.75
	Pulpers	1)	1)	1)
	Washer filters	-	-	1.50
	Yankee cylinders (dryers)	1)	1)	1)
<b>Rubber and plastic industry</b>	Extruders (plastic)	-	1.40	1.60
	Extruders (rubber)	-	1.50	1.80
	Rubber mills (2 in a row)	1.55	1.75	2.00
	Rubber mills (3 in a row)	-	1.50	1.75
	Warming mills	1.35	1.50	1.75
	Calenders	-	1.65	1.65
	Grinders	1.55	1.75	2.00
	Mixing mills	1)	1)	1)
	Sheeters	1.55	1.75	2.00
	Refiners	1.55	1.75	2.00
	Tubers	1)	1)	1)
<b>Waste water treatment</b>	Impeller areator	-	1.80	2.00
	Thickeners	1.15	1.25	1.50
	Vacuum filters	1.15	1.30	1.50
	Collectors	1.15	1.25	1.50
	Screw pump	-	1.30	1.50
	Brush areators	-	-	2.00

1) Contact SEW-EURODRIVE



#### Peak factor $F_F$

The peak factor  $F_F$  takes into account how often peak loads occur.

The permitted peak load depends on the frequency per hour and is calculated according to the following formula:

1. Based on torque

$$M_{K2\ zul} = \frac{2 \times M_{N2}}{F_F}$$

$M_{K2\ zul}$  = permitted peak torque at the gear unit output

$M_{N2}$  = gear unit nominal torque

$F_F$  = peak factor according to the following table

2. Based on power

$$P_{K1\ zul} = \frac{2 \times P_{N1}}{F_F}$$

$P_{K1\ zul}$  = permitted peak power at the gear unit input

$P_{N1}$  = gear unit nominal power

$F_F$  = peak factor according to the following table

	Frequency of peak load per hour					
	1...5	6...20	21...40	41...80	81...160	> 160
Peak factor $F_F$	1.00	1.20	1.30	1.50	1.75	2.00



The gear units may only be overloaded for a short period of time. Individual peak loads must not last for more than ten seconds.

### 5.3 Thermal rating $P_T$

The thermal rating  $P_T$  of a gear unit is the power that a gear unit can transmit continuously without exceeding a certain oil temperature. The thermal rating depends on the following factors:

- Type of lubricant used
- Ambient temperature
- Gear unit ratio
- Optional forced cooling methods (e.g. fan on HSS)
- Installation altitude of the gear unit (→ table, altitude factor  $f_1$ )
- Lubrication method of the gear unit (→ table, lubrication factor  $f_L$ )



For the following ambient conditions, the thermal rating can be directly read from the selection tables for

- ambient temperatures of 20°C or 40°C,
- natural cooling, or for cooling with fan (or two fans for MC2P units)
- altitudes < 1000 m ( $f_1 = 1$ )
- respective mounting positions
- splash (horizontal mounting position) or bath lubrication (vertical and upright mounting positions)

$$P_T = P_{TH} \times f_1 \times f_2 \times f_L \times f_T$$

$P_{TH}$  = Nominal thermal rating of the gear unit. The values given in the selection tables in chapters 10 + 11 depend on the ambient temperature and cooling method.

For  
 20°C:  $P_{TH [20]}$   
 40°C:  $P_{TH [40]}$   
 with cooling fan  
 20°C:  $P_{TH [20]}$   
 40°C:  $P_{TH [40]}$   
 with two cooling fans  
 20°C:  $P_{TH [20]}$   
 40°C:  $P_{TH [40]}$

$f_1$  = Altitude factor

$f_2$  = Mounting option factor  
 1.07 = shaft mounted with torque arm  
 1.00 = all other mounting options

$f_L$  = Lubrication factor  
 1.0 = splash and bath lubrication  
 1.1 = pressure lubrication

$f_T$  = Ambient temperature factor  
 The selection tables already take account of different ambient temperatures; the factor is therefore only relevant for ambient temperatures above 40°C. For ambient temperatures of 30°C, the thermal rating can be interpolated

$$P_{TH [30]} = \frac{P_{TH [20]} + P_{TH [40]}}{2}$$

**Altitude factor  $f_1$**

	Altitude H [m above sea level]				
	0	1000	2000	3000	4000
$f_1^{1)}$	1.00	0.95	0.91	0.87	0.83

1) Intermediate values must be interpolated



Consult SEW-EURODRIVE in case of deviating conditions.



**Ambient temperature factor  $f_T$**

Ambient temperature	20°C	30°C	40°C	50°C
$f_T$	1.0 <sup>1)</sup>	1.0 <sup>1), 2)</sup>	1.0 <sup>1)</sup>	Contact SEW-EURODRIVE

1) The selection tables in chapter 5 already take account of different ambient conditions.

2) Interpolation between PTH[20] and PTH[40] in chapters 10 + 11 is possible

#### 5.4 External radial and axial shaft loads

The permitted loads on the gear unit shaft depend on

- gear unit service factor
- required bearing lifetime
- direction of axial load (from or towards gear unit)
- application angle of radial load (rotating or at a specific position)
- position of radial load in relation to gear unit shaft shoulder
- relation of axial to radial load and vice versa

The limiting elements in a gear unit in terms of loads on the LSS depend on

- permitted load for the gear unit housing
- permitted force/stress of connection bolts of the gear unit foot or in the mounting flange
- permitted stress in the gear unit shaft
- minimum bearing life

Based on these factors, the selection tables in chapters 10 + 11 show a radial load value that applies to the following conditions:

- Radial load is applied on the middle of the shaft
  - HSS:  $F_{RE}$
  - LSS:  $F_{RA}$
- The application angle of the radial load is applied at the most unfavourable position
- The applied axial load is 0!
- The gear unit service factor is  $F_S = 1.5$  or higher
- The bearing life is equal or higher than a minimum value according to SEW standard

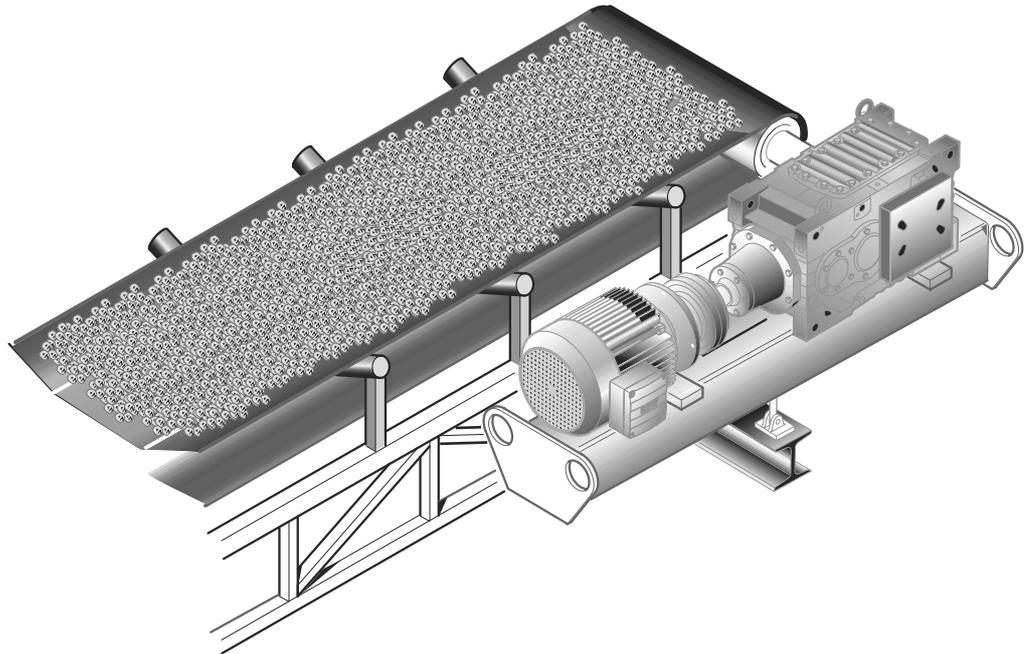


Contact SEW-EURODRIVE for deviating conditions. In many cases, higher loads can be applied.



### 5.5 Project planning example: Conveyor drive

Bulk material is to be transported from one point to another using a conveyor.



54029AXX

**Technical data and application conditions of bucket elevator gear units**

- Foot-mounted gear unit with hollow shaft
- Output speed  $n_2 = 35$  1/min
- Output torque  $M_{K2} = 9000$  Nm
- Maximum output torque  $M_{K2 \max} = 16$  kNm
- Maximum input power  $P_{K1 \max} = 61.4$  kW
- Operating time: 16 hours per day
- The gear unit is started up once per hour (frequency of maximum output torque)
- The gear unit is to be used in a large hall under very dusty conditions and an ambient temperature range of  $\vartheta_{\text{amb}} = 0^\circ\text{C} \dots 40^\circ\text{C}$
- Installation altitude  $H = 1000$  m
- Min. service factor  $F_S = 1.4$

**Technical data of AC motors**

- Input speed  $n_1 = 1500$  1/min
- Motor power  $P_m = 45$  kW



### Step 1: Calculating the gear ratio

Calculate the gear unit reduction ratio  $i$  using the following formula:

$$i = \frac{n_1}{n_2} = \frac{1500 \text{ 1/min}}{35 \text{ 1/min}} = 42.86$$

$i$  = ratio  
 $n_1$  = input speed  
 $n_2$  = required output speed

This value is used to specify the nominal gear ratio  $i_N = 45$  (→ chapters 10 + 11).

### Step 2: Calculating the operating power

The input power  $P_{K1}$  of the drive is calculated as follows using the output torque  $M_{K2}$  or output power  $P_{K2}$  as well as output speed  $n_2$  and efficiency  $\eta$ :

$$P_{K1} = \frac{M_{K2} \times n_2}{9.550 \times \eta} = \frac{9 \text{ kNm} \times 35 \text{ 1/min}}{9.550 \times 0.955} = 34.54 \text{ kW}$$

$P_{K1}$  = input power  
 $M_{K2}$  = output torque  
 $\eta$  = efficiency (→ chapter 5.1)

(where  $\eta = 0.955$  for three-stage gear units)

### Step 3: Specifying gear unit size and gear unit reduction ratio

The required nominal power of the gear unit  $P_{N1}$  is calculated using input power  $P_{K1}$  and service factor  $F_S = 1.4$  using the following formula:

$$P_{N1} \geq P_{K1} \times F_S$$

$$P_{N1} = 34.54 \text{ kW} \times 1.4 = 48.35 \text{ kW}$$

This value is used to select the gear unit size MC3RLHF04 from the selection tables (→ chapter 11).

The selection of the gear unit provides the following technical data:

- Nominal power  $P_{N1} = 55.8 \text{ kW}$
- Nominal gear ratio  $i_N = 45$  → exact gear ratio  $i_{ex} = 44.302$
- Nominal gear unit torque  $M_{N2} = 15 \text{ kNm}$



**Step 4:**  
**Calculating the permitted peak load**

The permitted peak power  $P_{K1\ zul}$  is calculated using nominal power  $P_{N1}$  and peak factor  $F_F$  (→ table, factor  $F_F$ ):

$$P_{K1\ zul} = \frac{2 \times P_{N1}}{F_F} = \frac{2 \times 48.35 \text{ kW}}{0.87} = 111.6 \text{ kW}$$

$P_{K1\ zul}$  = permitted peak power on gear unit  
 $P_{N1}$  = nominal power  
 $F_F$  = peak factor

The permitted peak torque  $M_{K2\ zul}$  is calculated using the nominal torque  $M_{N2}$  of the gear unit determined in step 3 and peak factor  $F_F$  (→ table, factor  $F_F$ ).

$$M_{K2\ zul} = \frac{2 \times M_{N2}}{F_F} = \frac{2 \times 15 \text{ kNm}}{0.87} = 30 \text{ kNm}$$

$M_{K2\ zul}$  = permitted peak torque on gear unit output  
 $M_{N2}$  = nominal gear unit torque  
 $F_F$  = peak factor

**Step 5:**  
**Checking the peak load**

The maximum operating power  $P_{K1\ max}$  must not exceed the permitted peak power  $P_{K1\ zul}$ !

$$P_{K1\ max} \leq P_{K1\ zul}$$

$$61.4 \text{ kW} \leq 111.6 \text{ kW}$$

or

The maximum output torque  $M_{K2\ max}$  must not exceed the permitted peak torque  $M_{K2\ zul}$ !

$$M_{K2\ max} \leq M_{K2\ zul}$$

$$16 \text{ kNm} \leq 30 \text{ kNm}$$

This means you can use the selected gear unit size.



## Project Planning for Gear Units

Project planning example: Conveyor drive

### Step 6: Calculating the thermal rating

$$P_T = P_{TH} \times f_1 \times f_2 \times f_L \times f_T = 29 \text{ kW} \times 1.0 \times 1.0 \times 1.0 = 29 \text{ kW}$$

$P_T$  = nominal thermal rating at 40°C of the gear unit  
 $P_{TH}$  = thermal rating  
 $f_1$  = altitude factor  
 $f_2$  = mounting option factor  
 $f_L$  = lubrication factor  
 $f_T$  = ambient temperature factor



Higher thermal ratings are possible when using synthetic lubricants and special oil seals. Contact SEW-EURODRIVE in such cases.

### Checking the thermal rating

The input power  $P_{K1}$  must not exceed the thermal rating  $P_T$  ( $P_{K1} \leq P_T$ ).  
Additional cooling is required if  $P_{K1} > P_T$ .

$$34.54 \text{ kW} > 29 \text{ kW}$$

→ Thermal rating not sufficient at 40°C

with one fan:

$$P_T = P_{TH[40]} \times f_1 \times f_2 \times f_L \times f_T = 72 \text{ kW} \times 1.0 \times 1.0 = 72 \text{ kW}$$

$P_T$  = nominal thermal rating at 40°C with one fan  
 $P_{TH}$  = thermal rating  
 $f_1$  = altitude factor  
 $f_2$  = mounting option factor



## 5.6 Project planning example: Mixer drive



5

53726AXX

### **Technical data and application conditions**

A liquid with constant density is to be agitated.

- Helical gear unit with parallel shafts
- Vertical mounting position, solid output shaft
- Required output speed  $n_2 = 51$  1/min
- Gear unit output power  $P_{K2} = 77$  kW
- Peak input torque  $M_{K1 \max} = 1.45$  kNm
- Operating time: 24 hours per day
- The gear unit is started twice per day (frequency of maximum input torque)
- The gear unit is operated outdoors under a protective roof. Ambient temperature range: 0°C ... 40°C, wind velocity approx. 3 m/s, normal humidity
- Installation altitude  $H = 500$  m
- Connected to a mixer shaft with flexible coupling; mixer shaft is supported externally, no radial and axial loads on gear unit shaft
- Foot mounted gear unit



### Technical data of AC motor

- Motor power  $P_M = 90$  kW
- Nominal speed:  $n_M = 1485$  1/min
- IEC size 280 M, flange  $\varnothing 550$  mm, shaft  $\varnothing 75$  mm x 140 mm

### Step 1: Calculating the gear ratio

Calculate the gear unit reduction ratio  $i$  using the following formula:

$$i = \frac{n_1}{n_2} = \frac{1485 \text{ 1/min}}{51 \text{ 1/min}} = 29.12$$

$i$  = ratio  
 $n_1$  = input speed  
 $n_2$  = required output speed

The value is used to specify the nominal gear ratio  $i_N = 28$  ( $\rightarrow$  chapter 10)

### Step 2: Calculating the operating power

The input power  $P_{K1}$  of the drive is calculated as follows using the output power  $P_{K2}$  or output torque  $M_{K2}$  as well as output speed  $n_2$  and efficiency:

$$P_{K1} = \frac{P_{K2}}{\eta} = \frac{77 \text{ kW}}{0.955} = 80.6 \text{ kW}$$

$P_{K1}$  = operating power  
 $P_{K2}$  = gear unit output power  
 $\eta$  = efficiency ( $\rightarrow$  chapter 5.1)

### Step 3: Specifying the service factor $F_S$

If the customer does not specify the service factor, it can be determined according to the table in chapter 5.2.

Field of application:           Agitators and mixers  
 Driven machine:                Agitators for liquids  
 Operating period per day:   > 10 h

$\rightarrow F_S = 1.5$



**Step 4:**  
**Specifying gear unit size and exact gear ratio**

The required nominal power of the gear unit  $P_{N1}$  is calculated using operating power  $P_{K1}$  and service factor  $F_S$  using the following formula:

$$P_{N1} \geq P_{K1} \times F_S$$

$$P_{N1} \geq 80.6 \text{ kW} \times 1.5 = 120.9 \text{ kW}$$

Approximate required nominal gear unit torque  $M_{N2}$ :

$$M_{N2} = \frac{P_{N1}}{n_2} = \frac{120.9 \text{ kW}}{51 \text{ 1/min}} \times 9.55 = 22.6 \text{ kNm}$$

$M_{N2}$  = approximate required nominal gear unit torque  
 $P_{N1}$  = required nominal power of the gear unit  
 $n_2$  = required output speed

Preselection on foldout page:

Torque class 25 kNm - Size 06 - Vertical - 1500 1/min

→ Chapters 10 + 11

- Nominal power: 134 kW
- Nominal ratio  $i_N = 28$  → Exact ratio  $i_{ex} = 29.61$   
→ Output speed  $n_2 = 1485 \text{ 1/min} / 29.61 = 50.1 \text{ 1/min}$
- Nominal gear unit torque:  $M_{N2} = 24.1 \text{ kNm}$
- Thermal rating at 40°C
  - 50 kW without fan
  - 115 kW with fan

**Step 5:**  
**Calculating the permitted peak torque**

The permitted peak torque  $M_{K2 \text{ zul}}$  is calculated using the nominal torque  $M_{N2}$  of the gear unit determined in step 4 and factor  $F_F$  (→ table, factor  $F_F$ )

$$M_{K2 \text{ zul}} = \frac{2 \times M_{N2}}{F_F} = \frac{2 \times 24.1 \text{ kNm}}{1} = 48.2 \text{ kNm}$$

$M_{K2 \text{ zul}}$  = permitted peak torque  
 $M_{N2}$  = nominal gear unit torque  
 $n_2$  = required output speed



### Step 6: Checking maximum output torque

The max. output torque  $M_{K2 \max}$  must not exceed the permitted output torque  $M_{K2 \text{ zul}}$ !

$$M_{K2 \max} \leq M_{K2 \text{ zul}}$$

with

$$M_{K2 \max} = M_{K1 \max} \times i_{\text{ex}} \times \eta = 1.45 \text{ kNm} \times 29.61 \times 0.955 = 41 \text{ kNm}$$

$M_{K2 \max}$  = maximum output torque  
 $M_{K1 \max}$  = maximum input torque  
 $i_{\text{ex}}$  = required output speed  
 $\eta$  = efficiency (→ chapter 5.1)

$$\rightarrow 41.0 \text{ kNm} \leq 48.2 \text{ kNm}$$

This means you can use the selected gear unit size

### Step 7: Calculating the thermal rating

$$P_T = P_{TH} \times f_1 \times f_2 \times f_L \times f_T$$

$P_T$  = thermal rating  
 $P_{TH}$  = nominal thermal rating  
 $f_1$  = altitude factor  
 $f_2$  = mounting option factor  
 $f_L$  = lubrication factor  
 $f_T$  = ambient temperature factor

With  $P_{TH}$  from chapters 10 and 11:

$$f_1, f_2, f_L, f_T = 1.0$$

$$\text{Without fan at } 40^\circ\text{C: } P_T = 50 \text{ kW}$$

$$\text{With fan at } 40^\circ\text{C: } P_T = 115 \text{ kW}$$

#### Result:

**Thermal rating without fan: 50 kW at an ambient temperature of 40°C**

**Thermal rating with fan: 115 kW at an ambient temperature of 40°C**

### Step 8: Checking the thermal rating

The operating power  $P_{K1}$  must not exceed the thermal rating of the gear unit.

$$P_{K1} \leq P_T$$

Without fan: 80.6 kW > 50 kW → thermal rating not sufficient!

#### Result:

**With fan: 80.6 kW < 115 kW → thermal rating sufficient, fan required!**

### Step 9: Selecting the gear unit accessories

- Oil expansion tank made from cast iron for bath lubrication
- Double radial seals on LSS (standard for vertical units)
- Motor adapter for IEC motor 280
- Elastic coupling type ROTEX 65 on input shaft; one hub mounted on gear unit, other hub bored and keywayed for connecting the respective motor
- Fan in motor adapter